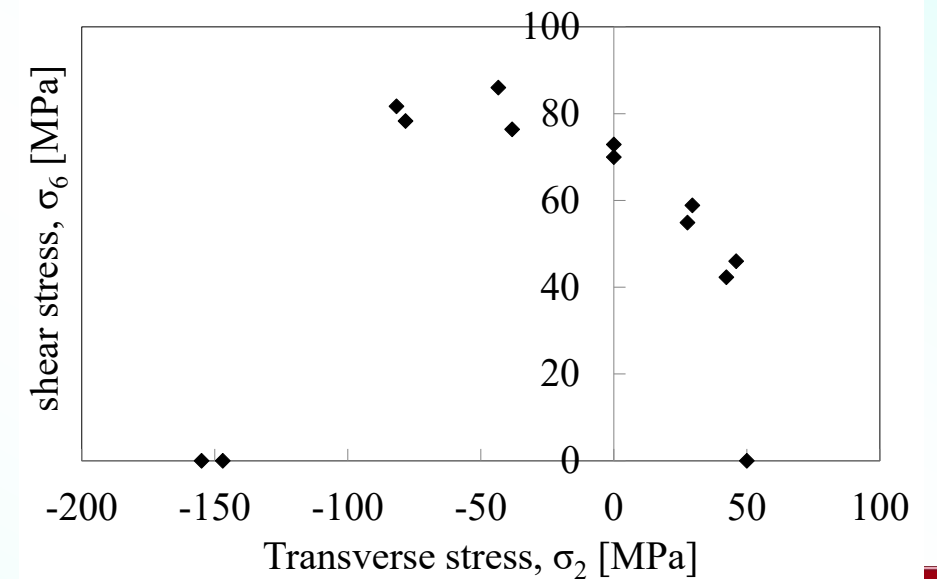


In-plane shear testing with tubular specimens

Marino Quaresimin, Paolo Andrea Carraro

Department of Management and Engineering, University of Padova

marino.quaresimin@unipd.it, paoloandrea.carraro@unipd.it



Tube configuration

How to obtain a pure shear stress (σ_6) on a tubular specimen?

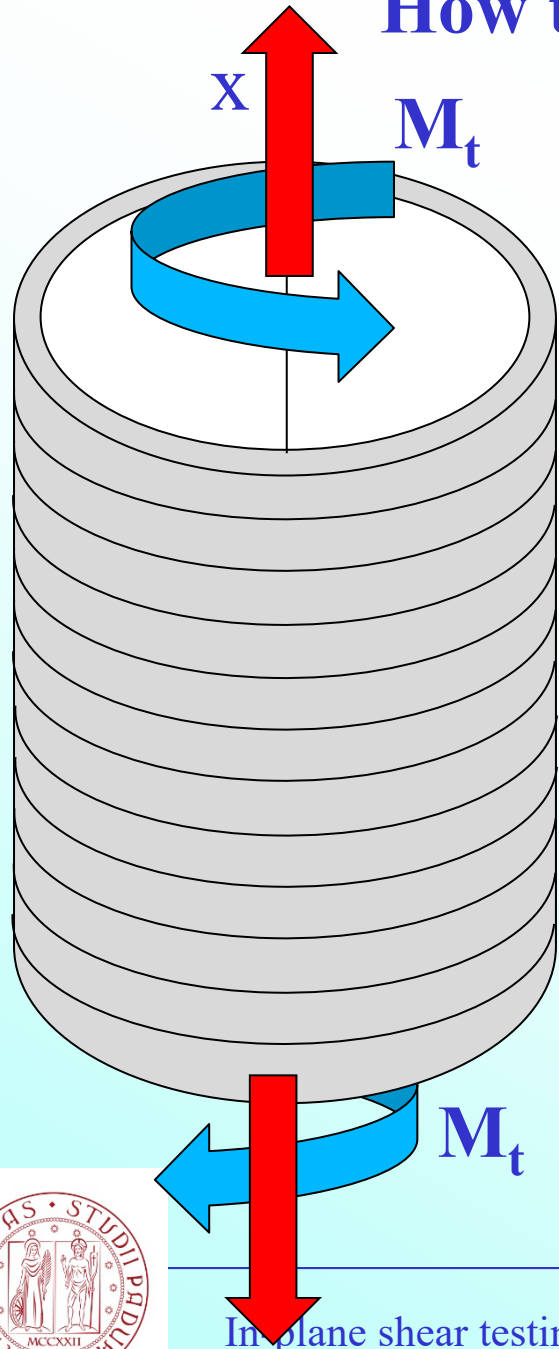
Tube under **torsion** with the UD fibres oriented either at 0° or at 90° with respect to the tube's axis (x-axis)

$0^\circ \rightarrow$ serious issues in manufacturing (large split formation during the demoulding phase)

90°

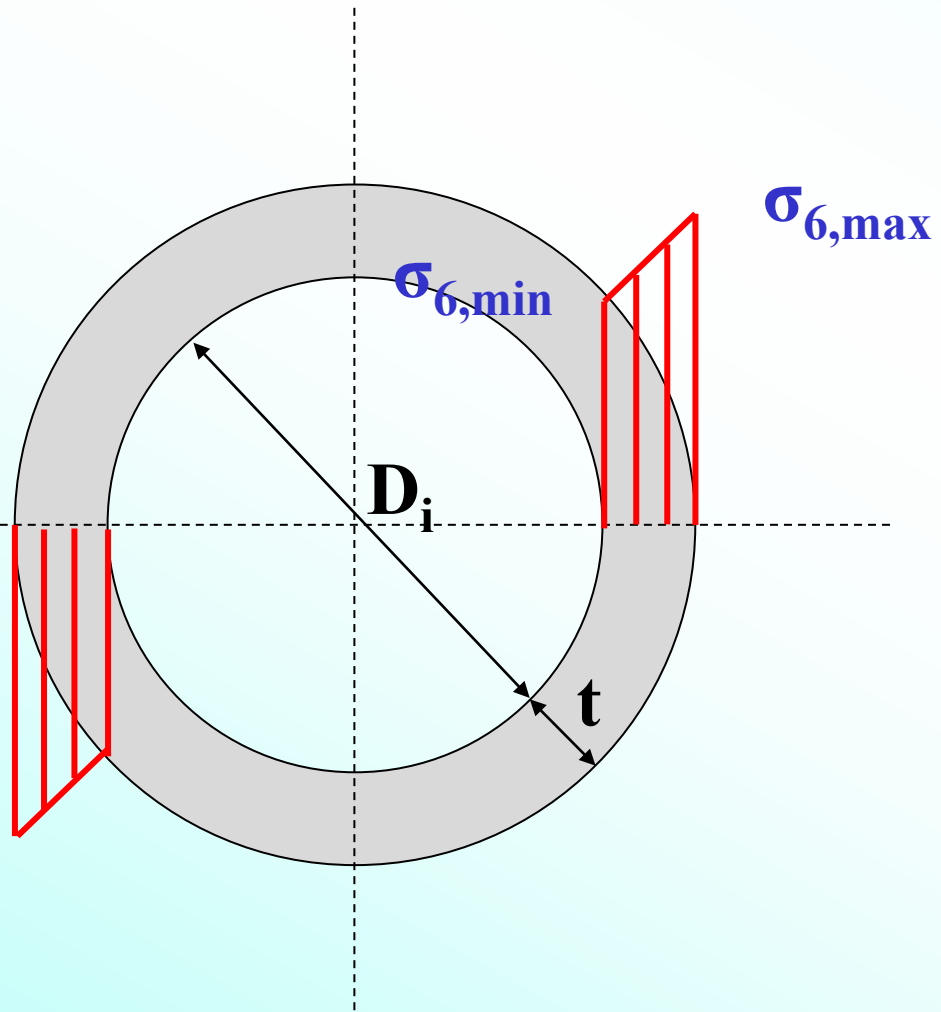
Combining **torsion** and **tension** loadings, possibility to obtain bi-axial stress states (σ_6 and σ_2) or (σ_6 and σ_1)

$$\lambda_1 = \frac{\sigma_2}{\sigma_1}, \lambda_2 = \frac{\sigma_6}{\sigma_1}, \lambda_{12} = \frac{\sigma_6}{\sigma_2}$$



In plane shear testing with tubular specimens –

Stress state



$$\frac{\sigma_{6,\max}}{\sigma_{6,\min}} = \frac{D_e}{D_i} = 1 + 2 \frac{t}{D_i}$$

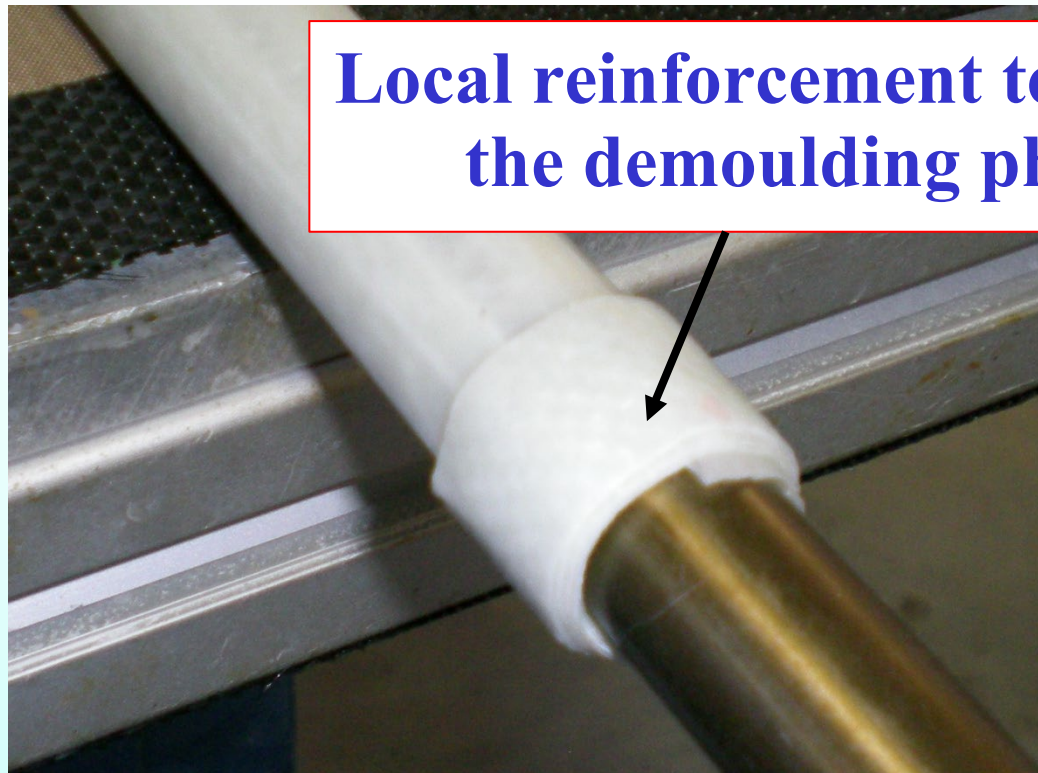


**The larger the tube and the thinner the thickness,
the lower the stress gradient and the effect of
the curvature!**

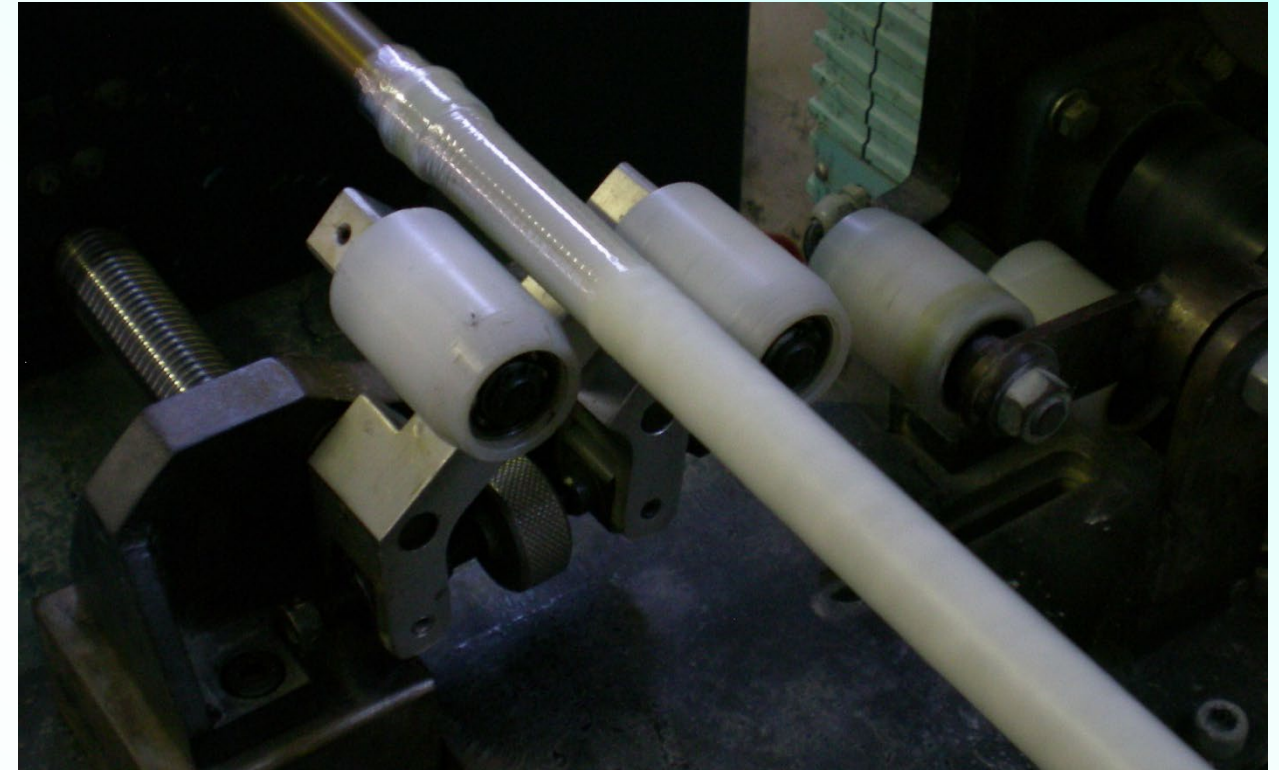
Quaresimin M., Carraro P.A., On the investigation of the biaxial fatigue behaviour of unidirectional composites, Composites Part B, 54 (2013) pp. 200–208.

Tube manufacturing

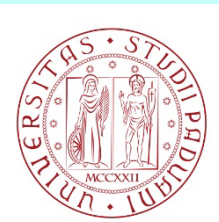
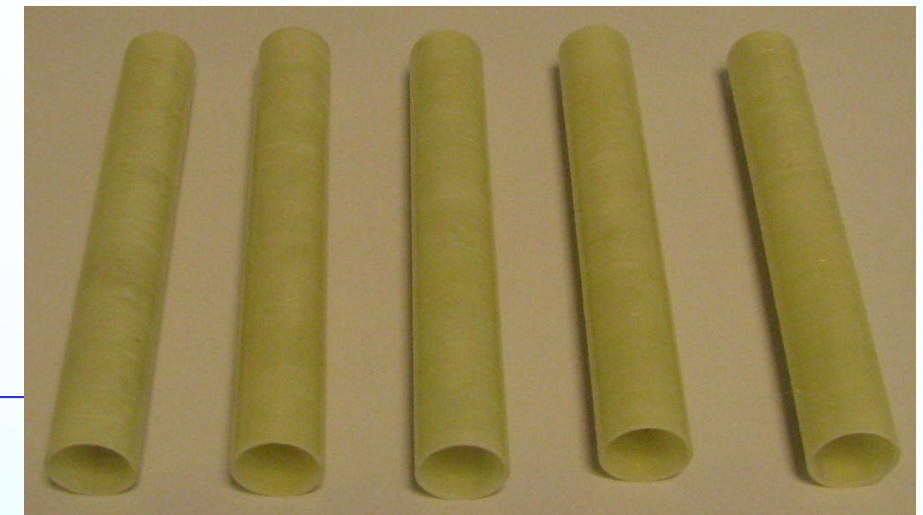
Mandrel wrapping + heat shrinking tape + autoclave moulding



Local reinforcement to help the demoulding phase

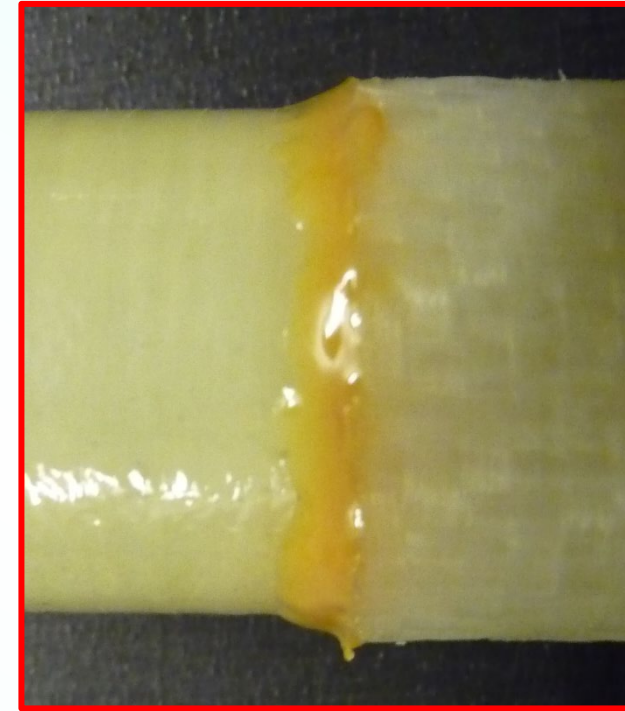
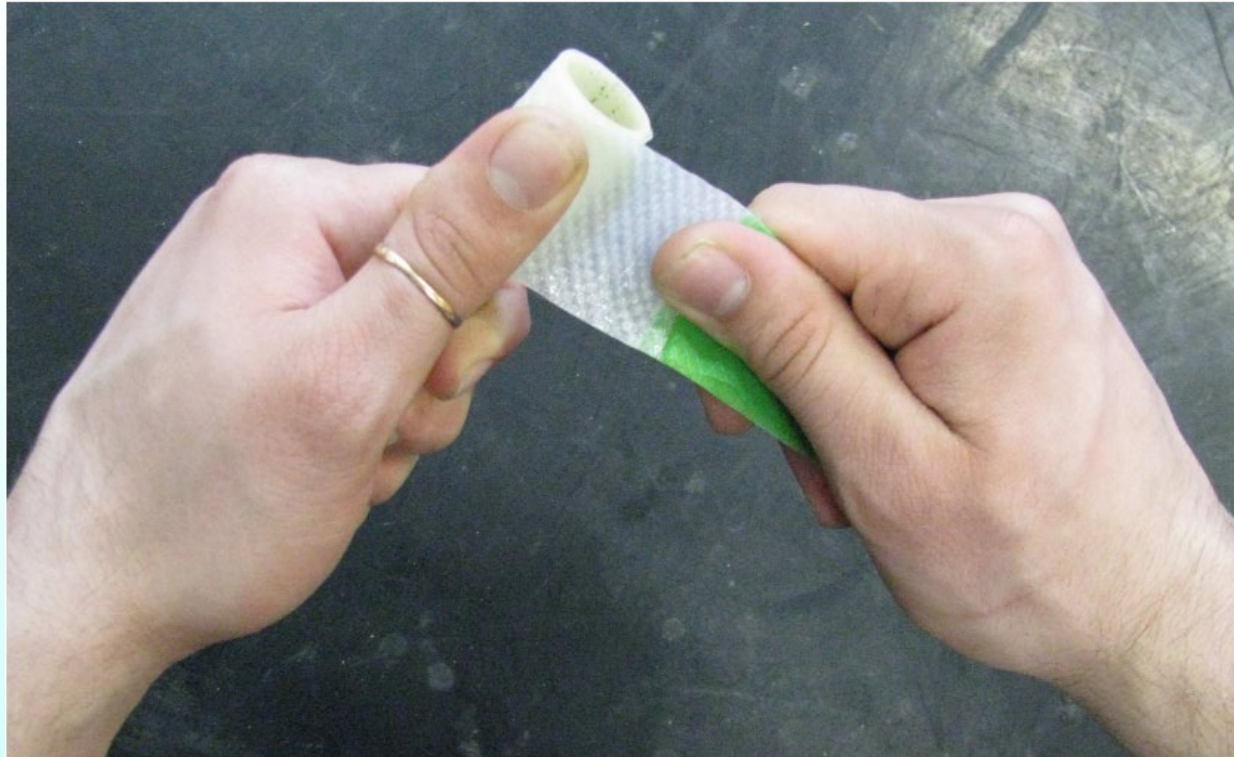


Typically, 1 meter long tubes can be manufactured and then cut into specimens of suitable length



Tabbing

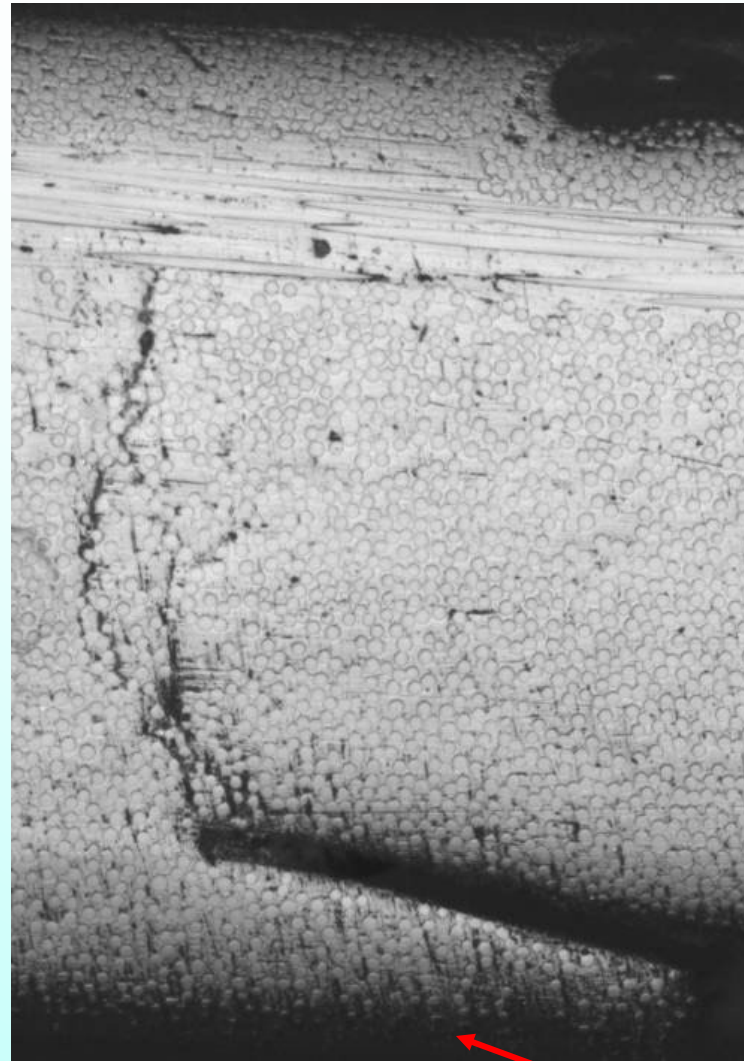
Pre-preg glass epoxy woven tabs rolled around the tube ends and cured in an oven



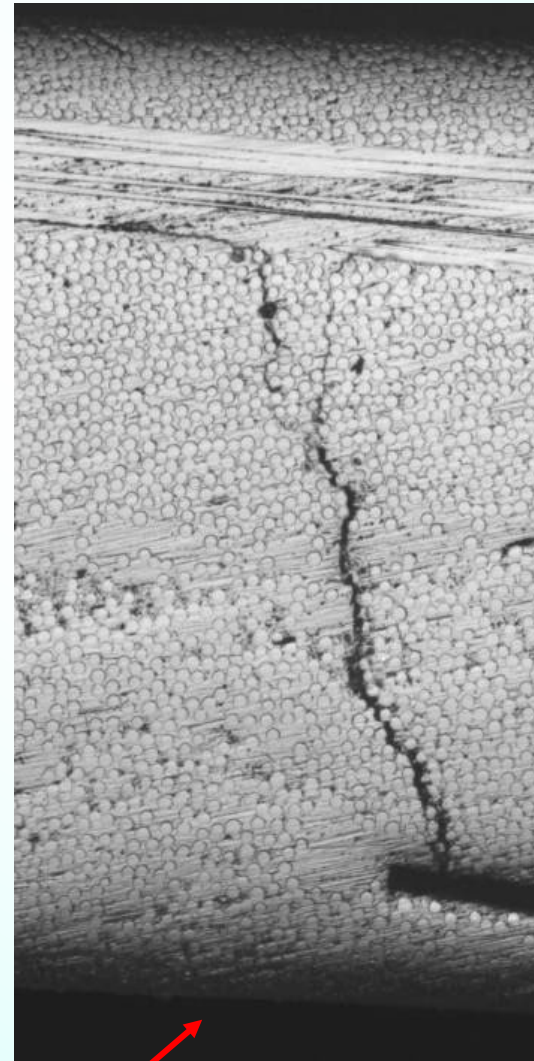
A resin fillet helps avoiding tab failures, particularly under compressive loads



Possible surface defects due to the heat shrinking tape

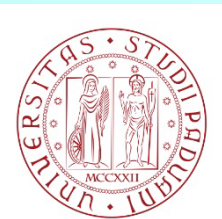
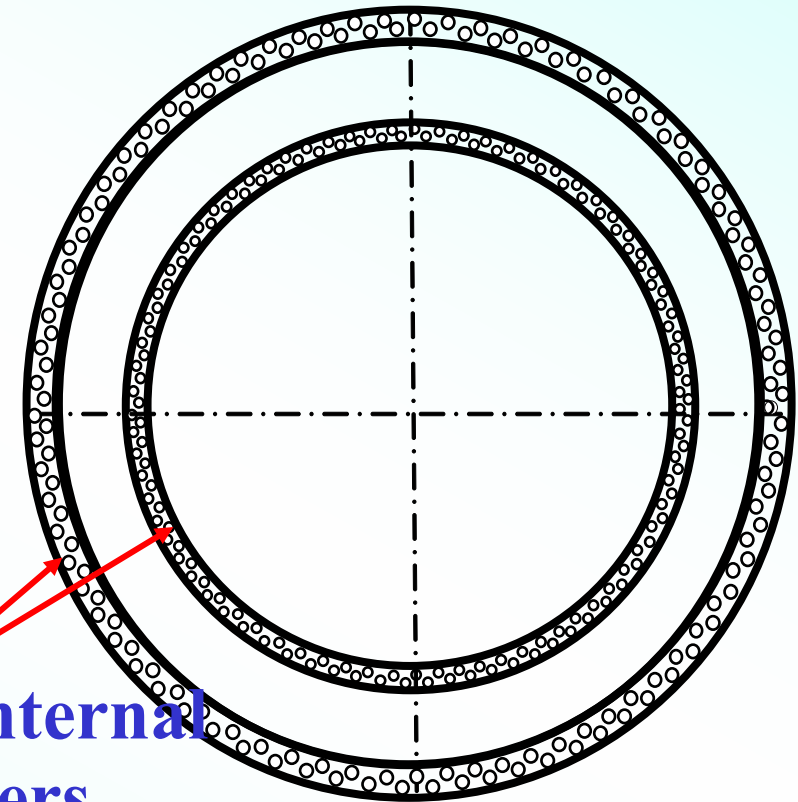


External surface

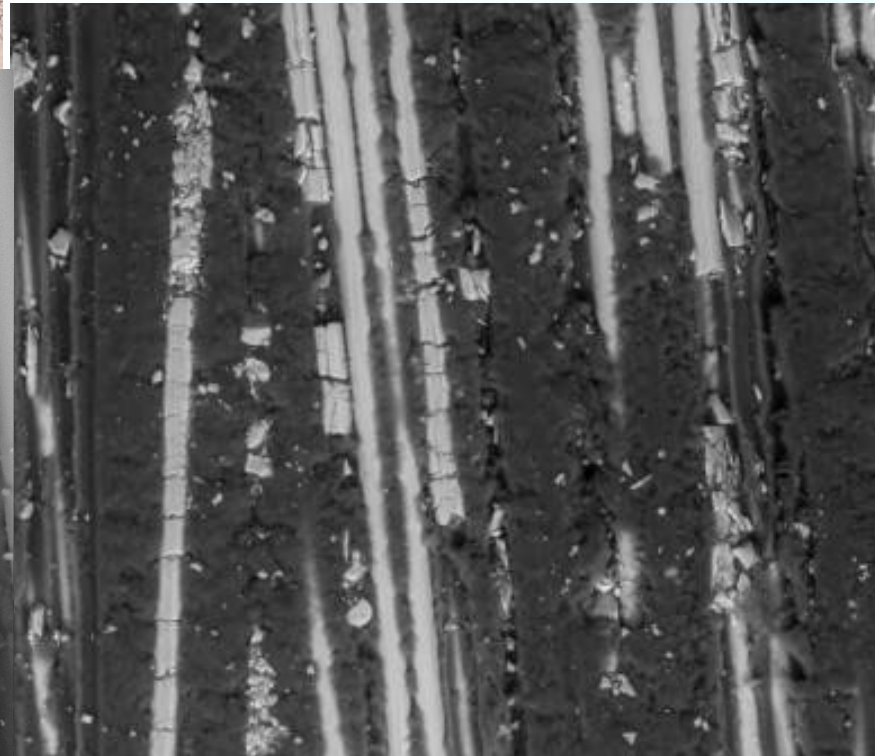
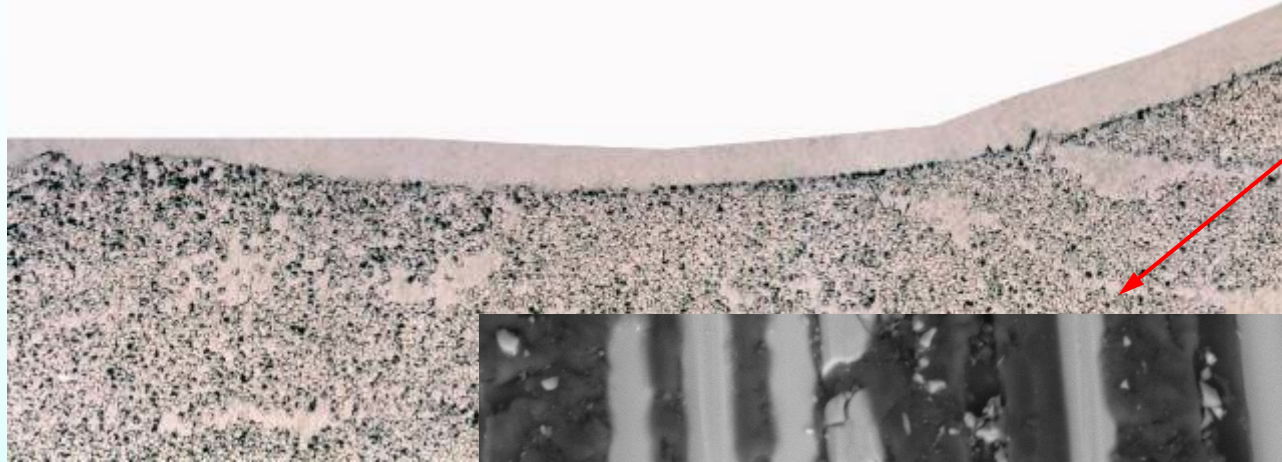


Thin external/internal fabric layers

They can be avoided by optimizing the pull and the feed of the heat shrinking tape, or using a cross-ply lay-up (focusing the attention on the crack initiation in the 90° plies only)



Tube machining: NOT OF HELP!



In-plane shear testing with tube

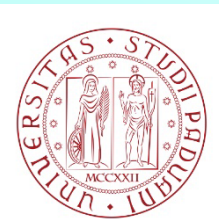
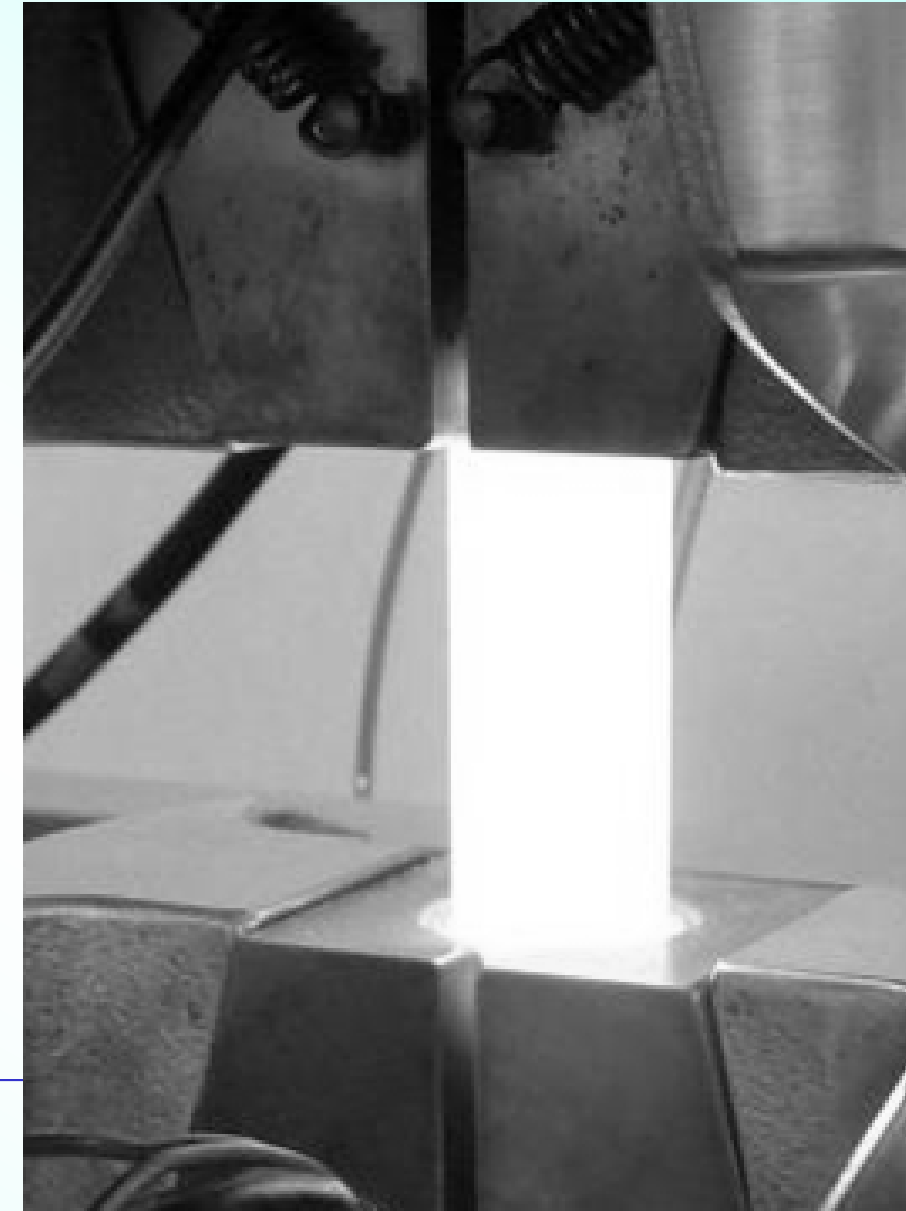
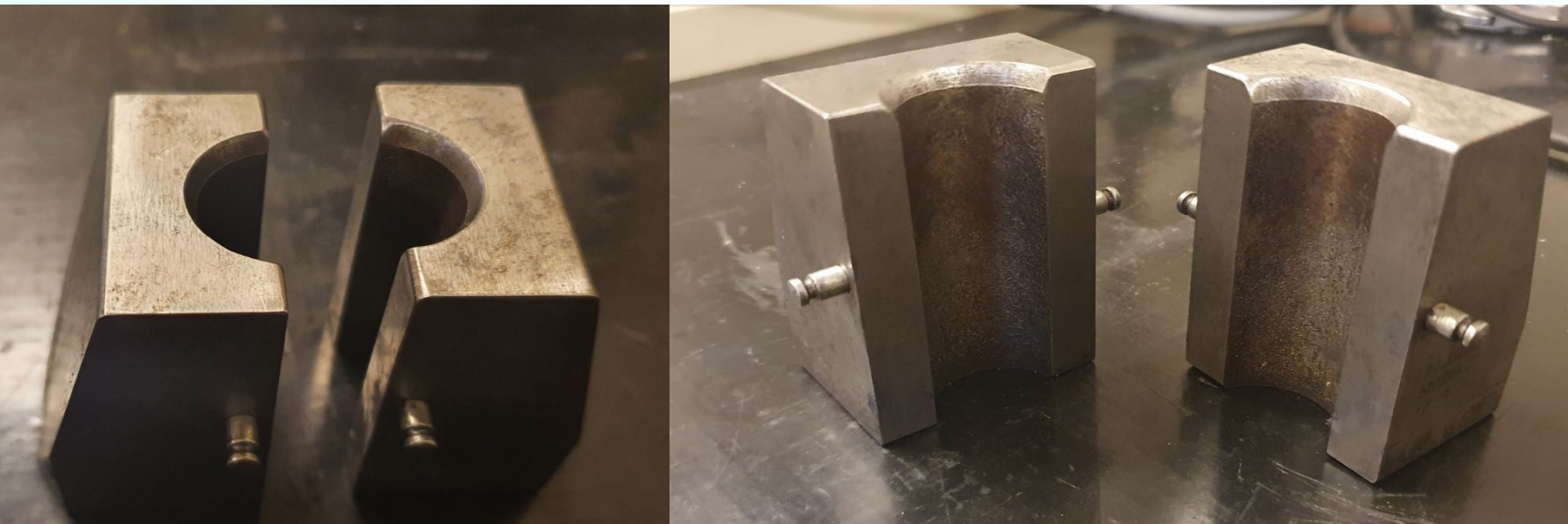
6/24/2009	HFW	WD	Mag	HV	Pressure	Det	50.0µm
10:59:24 AM	0.21 mm	10.7 mm	1300x	20.0 kV	1.00 Torr	SSD	

6/24/2009	HFW	WD	Mag	HV	Pressure	Det	100.0µm
10:56:36 AM	0.45 mm	10.6 mm	600x	20.0 kV	1.00 Torr	SSD	



Clamping

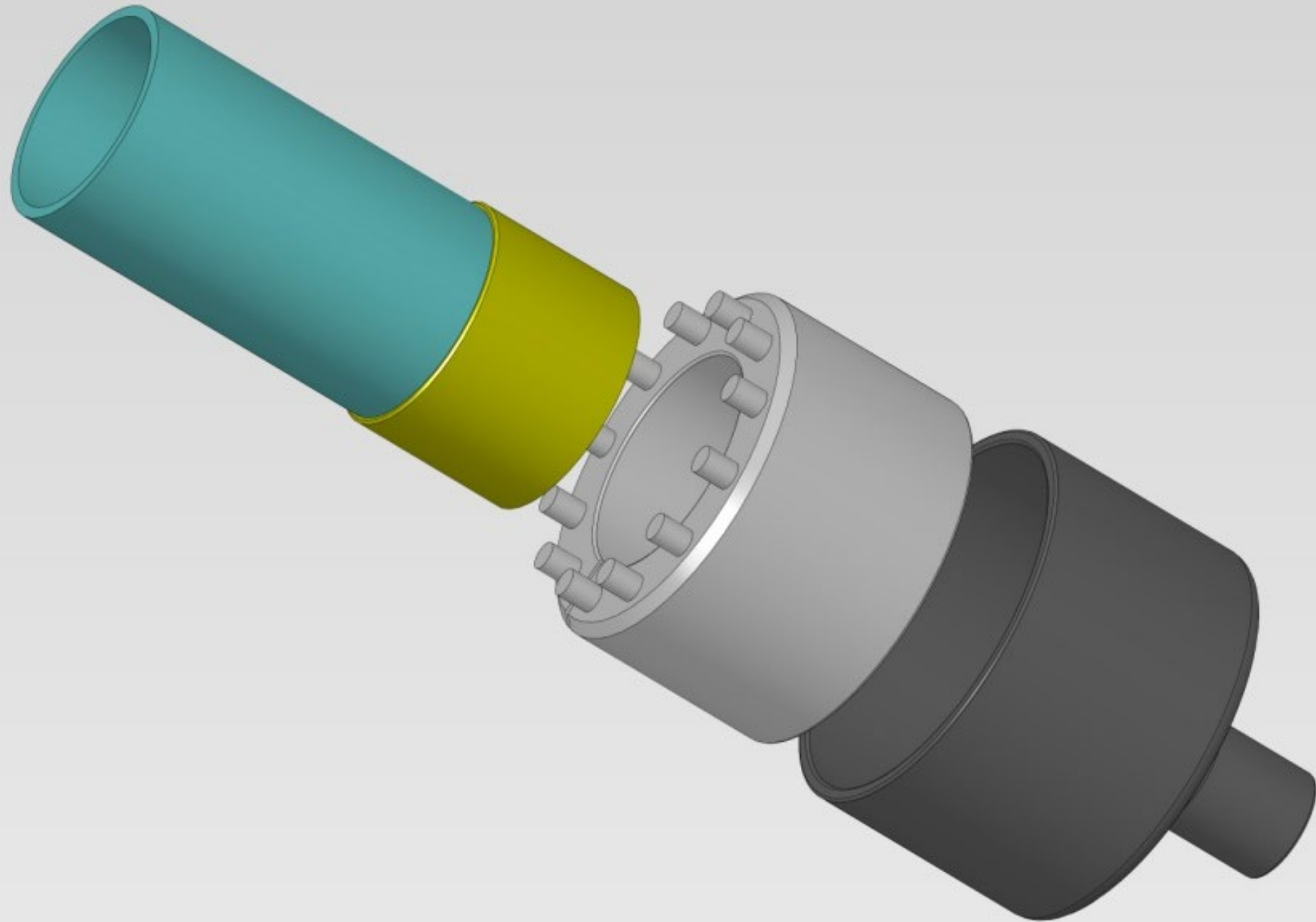
The correct clamping of tubular specimen requires cylindrical grips, which at the end control the tube diameter in the tab zone and the accuracy of the manufacturing required

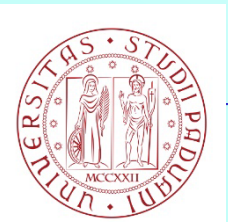


Clamping

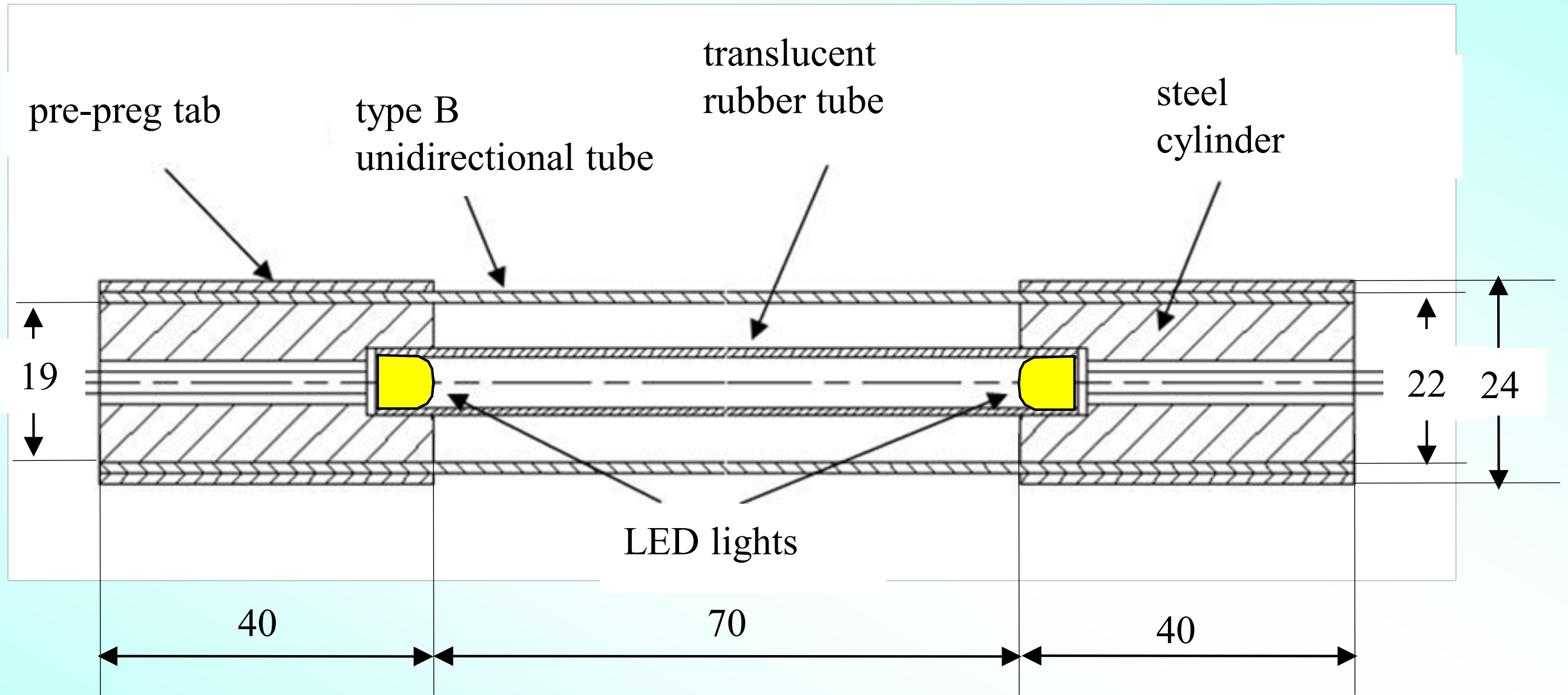


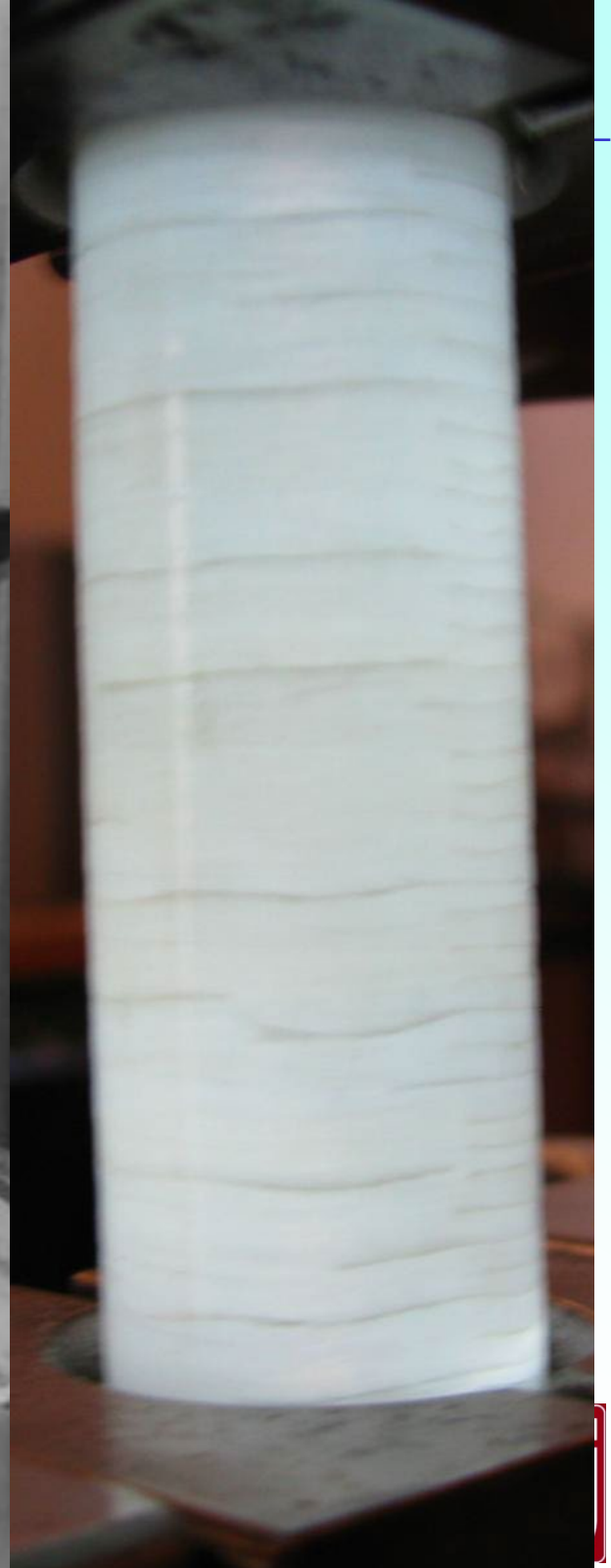
For large tubes, a dedicated clamping system is required, keyless friction locking devices can be used successfully



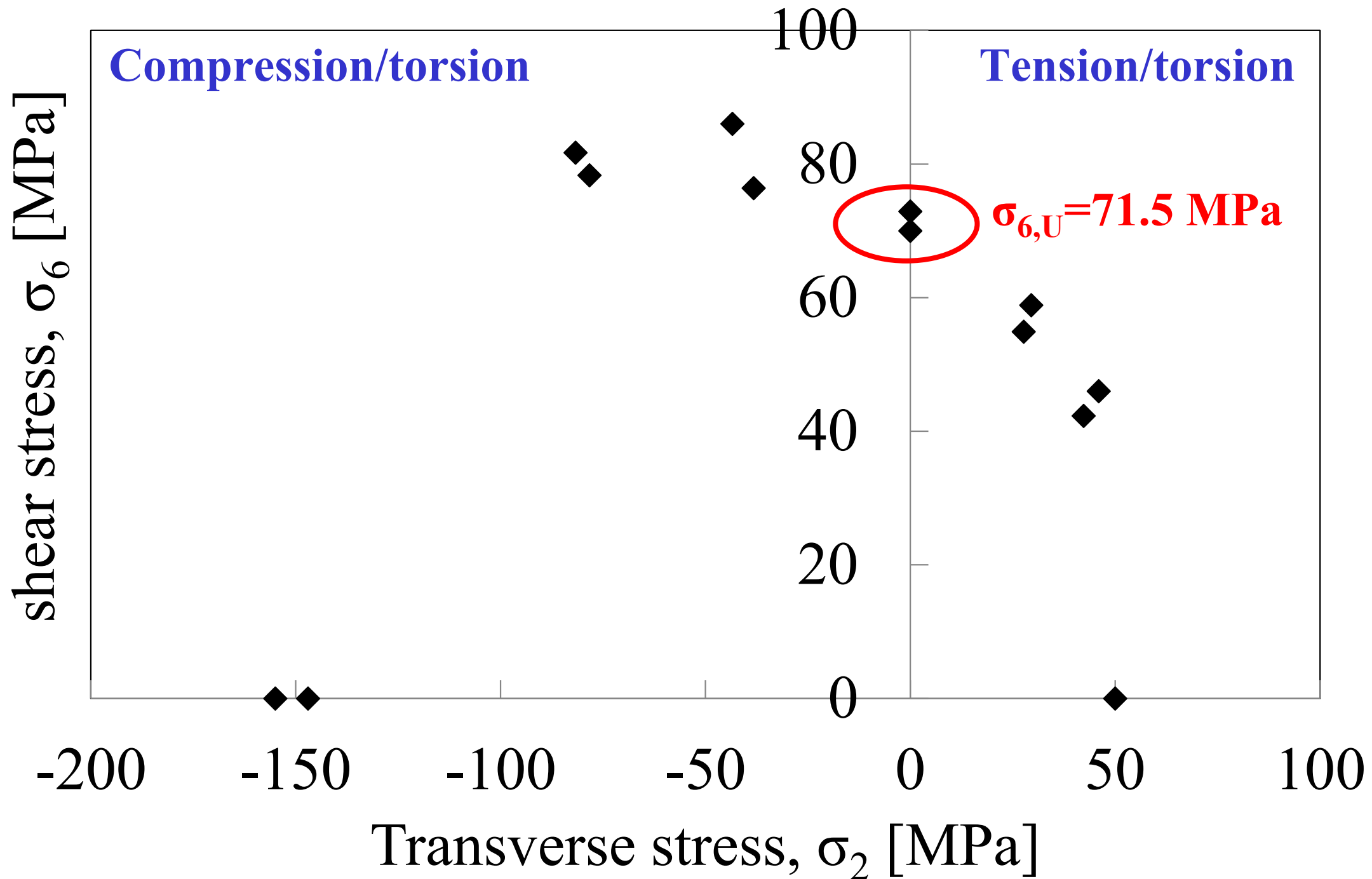


Internal light for damage analysis (G/E only)





Multiaxial proportional tests on 90° UD G/E tubes



Conclusions

Advantages of tubular specimens:

- **No free edges**
- **Pure shear** stress state under torsion (**direct assessment** of the shear strength, modulus and constitutive law)
- **No stress concentrations** and very **limited stress gradients**
- **Possibility of combining shear and transverse stress** using the same specimen configuration

Drawbacks:

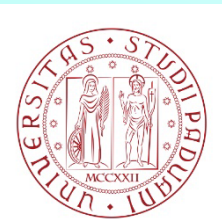
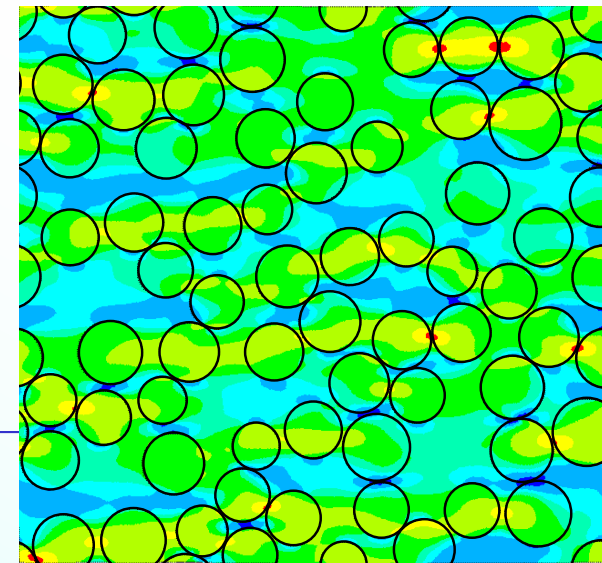
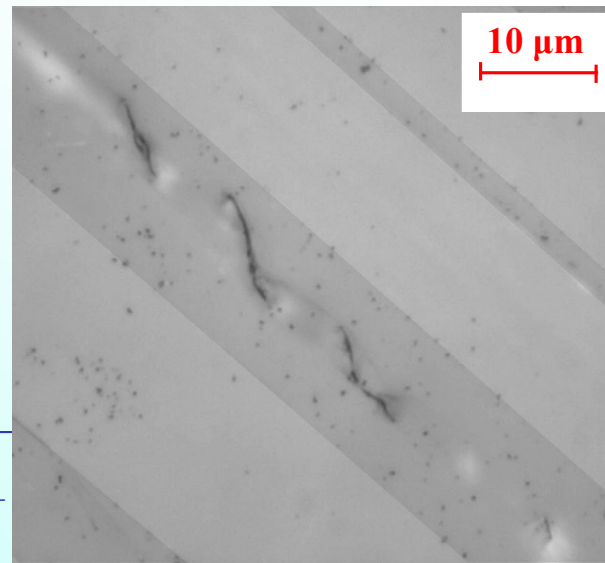
- **Not easy to manufacture**
- **Require a (tension)/torsion machine**



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